

## Heat Transfer with Internal Heat Generation

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ME 307: Heat Transfer Equipment Design

<http://zahurul.buet.ac.bd/ME307/>



## Modes of Heat Transfer

Conduction through a solid or a stationary fluid	Convection from a surface to a moving fluid	Net radiation heat exchange between two surfaces

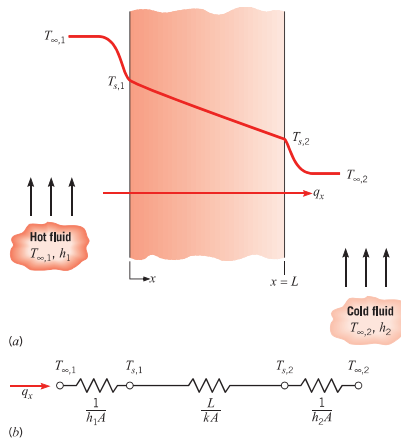
T946

### System with Internal Heat Generation

- Nuclear reactors
- Electric heater & conductors
- Exothermic chemical reactions

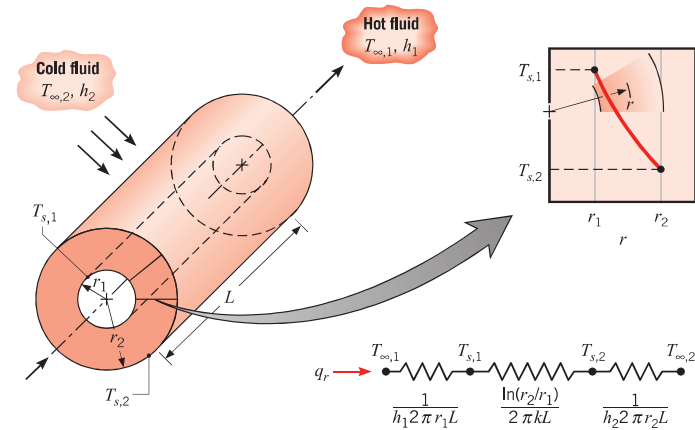


## Heat Conduction & Convection



T740

Heat transfer through a plane wall. (a) Temperature distribution. (b) Equivalent thermal circuit.

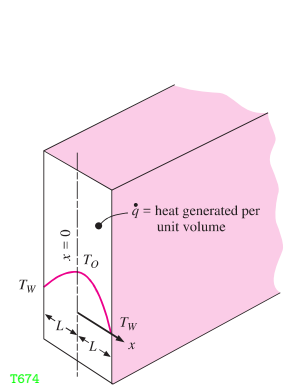


T741

Hollow cylinder with convective surface conditions.



## Plane Wall with Uniform Heat Generation



T674

► BC:  $T = T_w$  at  $x \pm L$

• DE:  $\frac{d^2 T}{dx^2} + \frac{\dot{q}_g}{k} = 0$

$\Rightarrow T(x) = -\frac{\dot{q}_g}{2k}x^2 + C_1x + C_2$

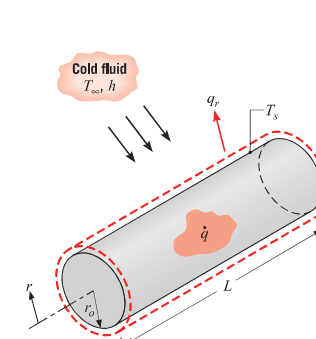
$$T(x) = T_w + \frac{\dot{q}_g}{2k}L^2 \left[ 1 - \left(\frac{x}{L}\right)^2 \right]$$

• if  $T(x = 0) = T_0$ :

$$T_0 = T_w + \frac{\dot{q}_g}{2k}L^2$$

$$\frac{T - T_w}{T_0 - T_w} = 1 - \left(\frac{x}{L}\right)^2$$

## Radial System with Internal Heat Generation



T676

► BCs:

•  $T(r_0) = T_s$

•  $\frac{dT}{dr} \Big|_{r=0} = 0$

• DE:  $\frac{1}{r} \frac{d}{dr} \left( r \frac{dT}{dr} \right) + \frac{\dot{q}_g}{k} = 0$

$\Rightarrow T(r) = -\frac{\dot{q}_g}{4k}r^2 + C_1 \ln r + C_2$

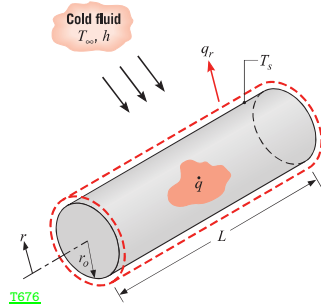
$$T(r) = T_s + \frac{\dot{q}_g}{4k}r_0^2 \left[ 1 - \left(\frac{r}{r_0}\right)^2 \right]$$

• if  $T(r = 0) = T_0$ :

$$T_0 = T_s + \frac{\dot{q}_g}{4k}r_0^2$$

$$\frac{T(r) - T_s}{T_0 - T_s} = 1 - \left(\frac{r}{r_0}\right)^2$$

contd. ...



T676

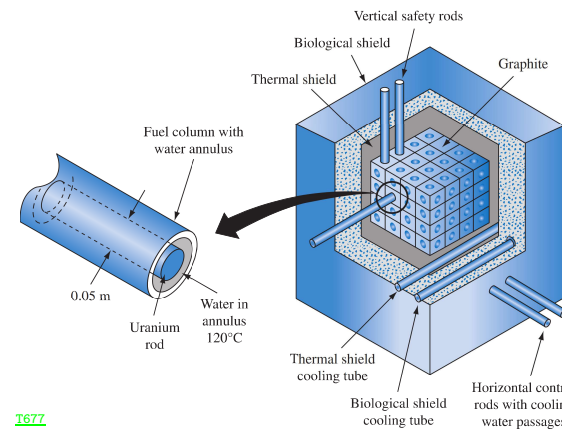
• Applying an overall energy balance:

$$\dot{q}_g(\pi r_0^2 L) = h(2\pi r_0 L)(T_s - T_\infty)$$

$$T_s = T_\infty + \frac{\dot{q}_g r_0}{2h}$$

$$T_{max} = T_0 = T_s + \frac{\dot{q}_g}{4k}r_0^2 = T_\infty + \frac{\dot{q}_g r_0}{4h} \left( 2 + \frac{hr_0}{k} \right)$$

Example: ▷ Heat is generated at  $7.5 \times 10^7 \text{ W/m}^3$  in nuclear reactor uranium rods of 0.05 m diameter. These rods are jacketed by an annulus in which water at  $120^\circ\text{C}$  is circulated. If  $h_{av} = 55000 \text{ W/m}^2 \text{ K}$ , and for uranium,  $k = 29.5 \text{ W/m K}$ , determine the center temperature of the uranium fuel rods.



T677

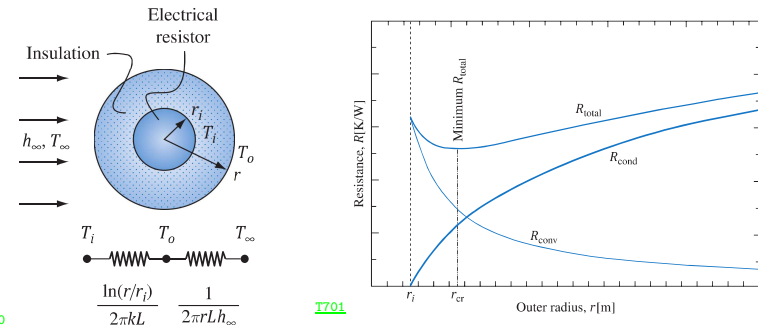
•  $T_s = 137.05^\circ\text{C}$  ◀

•  $T_0 = 534.29^\circ\text{C}$  ◀

Example: ▷ A current of 200 A is passed through a stainless-steel wire [ $k = 19 \text{ W/m}^\circ\text{C}$ ] 3 mm in diameter. The resistivity of the steel may be taken as  $70 \mu\Omega\text{cm}$ , and the length of the wire is 1 m. The wire is submerged in a liquid at  $110^\circ\text{C}$  and experiences a convection heat-transfer coefficient of  $4 \text{ kW/m}^2\text{C}$ . Calculate the center temperature of the wire.

- $\dot{q}_g = 560.39 \text{ MW/m}^3 \blacktriangleleft$
- $T_o = 231.66^\circ\text{C} \blacktriangleleft$

## Critical Thickness of Insulation



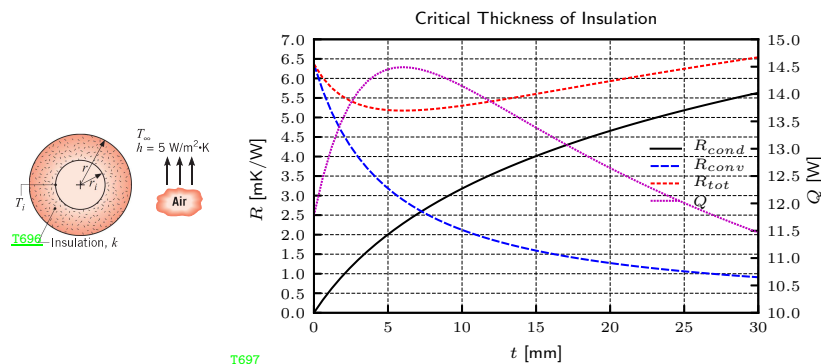
T700

T701

- $R_{total} = R_{cond} + R_{conv} = \frac{\ln(r/r_i)}{2\pi kL} + \frac{1}{2\pi rLh_\infty}$
- For maximum heat loss,  $\frac{dR_{total}}{dr} = \frac{1}{2\pi krL} - \frac{1}{2\pi r^2Lh_\infty} = 0 \rightarrow r = \frac{k}{h_\infty}$

*Critical thickness of insulation,  $r_{cr} = \frac{k}{h_\infty}$*

Example: ▷ Critical thickness of insulation,  $k = 0.055 \text{ W/mK}$ ,  $r_i = 5 \text{ mm}$ ,  $T_i = 100^\circ\text{C}$ ,  $T_\infty = 25^\circ\text{C}$ .



T697

- $r_{cr} = k/h = 11 \text{ mm}$ ,  $t = r_{cr} - r_i = 6 \text{ mm} \blacktriangleleft$
- $Q = 14.5 \text{ W} \blacktriangleleft$